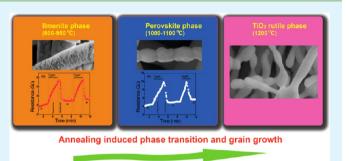
Investigation of Change in Surface Area and Grain Size of Cadmium Titanate Nanofibers upon Annealing and Their Effect on Oxygen Sensing

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Supporting Information

ABSTRACT: We have investigated the phase changes in CdTiO₃ nanofibers as the annealing temperature of nanofibers was increased from 600 to 1200 °C. The nanofibers annealed at 600 °C were ilmenite with a very small amount of CdO. Upon annealing at 950 °C, CdO was completely removed. Annealing at 1000 °C yielded pure perovskite nanofibers, and at temperatures above 1100 °C rutile TiO₂ nanofibers were obtained. Brunauer–Emmett–Teller (BET) analysis showed that with increase in annealing temperature the surface area of nanofibers was decreased. The nanofibers annealed at 600 °C have the higher surface area of ~9.41 m²/g. Then oxygen



sensors using CdTiO₃ nanofibers annealed at 600 °C (ilmenite) and 1000 °C (perovskite) were fabricated. The sensitivity of the ilmenite nanofibers sensor was 2 times than that of the perovskite nanofibers sensor. The response and recovery times were 120 and 23 s, respectively, for the ilmenite nanofibers sensor, whereas response and recovery times were 156 and 50 s, respectively, for the perovskite nanofibers sensor. Better oxygen characteristics of ilmenite nanofibers are attributed to their large surface area and porosity. Therefore, we believe that ilmenite CdTiO₃ nanofibers are potential candidates to develop practical oxygen sensors.

KEYWORDS: CdTiO₃, electrospinning, nanofibers, phase transformation, oxygen sensor

1. INTRODUCTION

Titanium-based oxides are of great interest due to their diverse applications such as humidity sensors, gas sensors, microelectronic devices, and photocatalytic cells.^{1,2} Various synthesis techniques such as hydrothermal crystallization,³ sol–gel,⁴ sputtering,⁵ and electrospinning^{1,6} have been used to prepare nanostructures of these oxides. Spray pyrolysis has also been used to synthesize TiO₂ thin films and flower-like nanostructures.^{7,8} Cadmium titanate (CdTiO₃), one of these oxides, has excellent gas sensing, dielectric, and optical properties.^{9,10}

Oxygen sensing and leakage from industrial installations is considered a most critical problem to be resolved related to human health, aquatic life, and environmental issues.^{6,11} Oxygen leakage may lead to fire and explosion hazards in hyperbaric chambers used in medical treatment, food preservation and packing, steel works, and chemical plants.^{12,13} Moreover, the pure oxygen is very reactive, and due to its specific physical properties (colorless, odorless, and tasteless), it cannot be detected by human senses. Therefore, many efforts have been made to produce low cost, faster, and linear oxygen gas sensors based on semiconductor nanostructures. These semiconductor gas sensors detect an oxidizing or reducing gas by observing change in electrical resistance. The surface area, size, and shape of nanostructures play an important role in the development of a gas sensor.¹⁴ The nanofibers have a larger specific surface area than that of the micrometer-sized powders.¹⁵ Further, the porous nature of nanofibers facilitates the gas diffusion, and chain like nanofibers provide a continuous path for charge transport.^{16–18} This unique morphology increases the electrochemical reaction sites. As a result, the sensor based on nanofibers morphology exhibits improved sensitivity, lower detection limits, and a faster response to the change in the gas concentration.

Titanium based oxides have been used to fabricate gas sensors due to their wide band gap (3.3-4.0 eV).^{19,20} Castaneda reported the effect of palladium coatings on oxygen sensors of TiO₂ thin films prepared by the ultrasonic spray pyrolysis method.²¹ He also investigated the effect of colloidal silver nanoparticles on the performance of the flower-like titanium-dioxide-nanostructure-based oxygen sensor.²² Moreover, it has been observed that the addition of rhodium to TiO₂ films increases their sensitivity.²³ Furthermore, gas sensors based on nanofibers of various titanates have been investigated in recent years as well. Hu et al. reported a low temperature SrTiO₃ oxygen sensor by recording DC currents.¹¹ Choi et al. studied sensing properties of electrospun SrTi_{0.65}Fe_{0.35}O_{3- δ}

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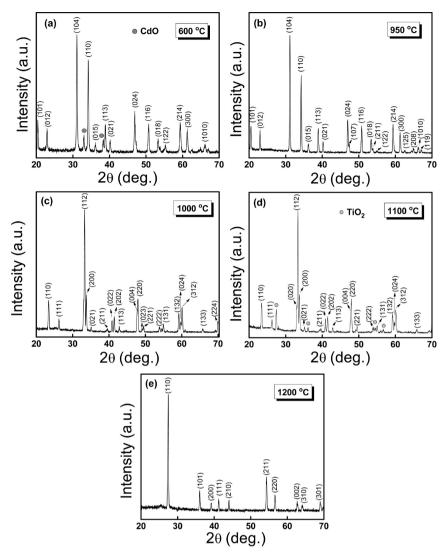


Figure 1. XRD patterns of the products obtained after heating at (a) 600 °C, (b) 950 °C, (c) 1000 °C, (d) 1100 °C, and (e) 1200 °C.

nanofibers using DC electrical measurements.⁶ Ding et al. studied the gas sensors based on electrospun nanofibers and showed that nanofiber-based sensors have much higher sensitivity and quicker responses to target gases.²⁴

However, there are no studies on gas sensing characteristics of CdTiO₃ nanofibers. Furthermore, the effect of annealing on change in surface area, grain size, and sensing properties of CdTiO₃ nanofibers has not been investigated as well. Therefore, we investigate the changes in surface area and grain size of CdTiO₃ nanofibers upon annealing and its effect on oxygen sensing. Annealing at 600 °C, 950 °C, 1000 °C, and >1100 °C resulted in ilmenite CdTiO₃ nanofibers with a very small amount of CdO, pure ilmenite CdTiO₃ nanofibers, pure perovskite CdTiO₃ nanofibers, and rutile TiO₂ nanofibers, respectively. BET analysis showed that with an increase in annealing temperature, the surface area of nanofibers decreases. The CdTiO₃ nanofibers annealed at 600 °C (ilmenite) and 1000 °C (perovskite) were then used to fabricate oxygen sensors. Better oxygen characteristics of ilmenite nanofibers were observed as compared to the perovskite nanofiber sensor and are attributed to their large surface area and porosity.

2. MATERIALS AND METHODS

2.1. Nanofiber Synthesis and Characterization. $CdTiO_3$ nanofibers were prepared via the electrospinning technique.¹⁰ Cadmium acetate (Cd(CH₃COO)₂·2H₂O > 98%), titanium tetraisopropoxide (Ti(CH₃)₂CHO)₄ > 99%), acetic acid (CH₃COOH >98%), ethanol (C₂H₃OH >98%), and polyvinyl-pyrrolidone (PVP; $M_W = 1$ 300 000) were purchased from Sigma-Aldrich. All chemicals were used without any further purification and were of analytical grade. Solution one was prepared by adding 2 g of cadmium acetate in 4 mL of acetic acid at room temperature. Titanium tetraisopropoxide was then mixed dropwise in solution 1. The second solution was prepared by adding 0.5 g of PVP in 4 mL of ethanol under stirring for 15 min. To get a homogeneous solution of optimum viscosity, these two solutions were mixed and vigorously stirred for 3 h in a glovebox.

The final solution was loaded in a syringe with a 24-gauge needle. The needle and collector plates were connected to the positive and negative terminals of a high voltage power supply of 10 kV, respectively. The nanofibers were collected on aluminum foil placed on the collector plate. The distance between the tip of the needle and collector plate was 7 cm, resulting in an electric field of 1.42 kV/cm. The whole process of electrospinning was carried out in an open environment. The as-spun nanofibers were dried in an oven at 80 °C for 3 h. Finally, PVP was burned to obtain pure CdTiO₃ nanofibers by annealing at different temperatures from 600 to 1200 °C for 3 h at a heating rate of 5 °C/min.

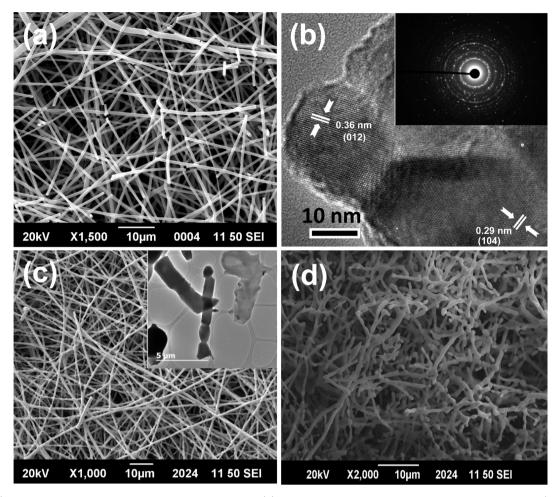


Figure 2. (a) SEM image of CdTiO₃ nanofibers annealed at 600 °C. (b) HRTEM image of CTiO₃ nanofibers annealed at 600 °C (inset shows the SAED image). (c) SEM image of CdTiO₃ nanofibers annealed at 1000 °C (inset shows the TEM image). (d) SEM image of CdTiO₃ nanofibers annealed at 1200 °C.

2.2. Device Fabrication. To study the oxygen sensing properties, suspension of the CdTiO₃ nanofibers with an ilmenite phase (annealed at 600 °C) and perovskite phase (annealed at 1000 °C) in isopropanol was prepared with a weight ratio of 1:100. The suspension was placed in an ultrasonic bath for 30 min to disperse nanofibers uniformly in isopropanol. Two different devices were then fabricated on a glass substrate using ilmenite and perovskite nanofibers. First of all, lithography and thermal evaporation were used to define electrical contacts with a separation of ~80 μ m between them. Chromium (20 nm) followed by gold (80 nm) was evaporated for the contacts. Subsequently, nanofibers were deposited between the electrical contacts on a glass substrate by dropping a known volume of nanofiber suspension using a micropipet. As a result, multiple nanofibers were randomly deposited between the electrodes. Since the same volume of suspension was used, the number of nanofibers between electrical contacts was approximately the same in both devices.

2.3. Characterization. X-ray diffraction (XRD) analysis was performed using a D8 Discoverer HR-XRD BRUKER (Germany) with Cu K α radiation (λ = 1.5418 Å). Field emission scanning electron microscope (SEM) and transmission electron microscope (TEM) images were obtained on a JSM-6490LA SEM and a Jeol 2010 (200 kV) TEM Japan, respectively. BET analysis was performed on a Micromeretics ASAP 2020 apparatus. The BET specific surface area, pore volume, and pore size distribution of the annealed samples at 600 and 1000 °C were determined by N₂ adsorption-desorption isotherms at 77 K shown in Figure 3a and b. Both the annealed samples were degassed at 393 K for 6 h under a vacuum (3 × 10⁻¹ Torr) before recording their BET isotherms. The cumulative pore

volume was calculated from the amount of nitrogen adsorbed up to a relative pressure, P/P_{0} , of 0.99, assuming all the pores are filled. The working principle of BET surface area analysis can be found elsewhere.²⁵

Oxygen sensing (99.9% pure) was studied using both devices at different gas flow rates. Oxygen flow was regulated by a 65 mm EW-32044-00 Cole-Parmer flow meter. It can precisely control the oxygen gas flow in the range of 0.44 to 5.05 sccm (standard cubic centimeter per minute). The performance of the gas sensing device was evaluated by taking DC measurements. Current–voltage (I-V) measurements were performed using a Keithley 2400 source meter. The complete setup for the gas sensor was maintained at ~25 °C in a clean-room environment.

3. RESULTS AND DISCUSSION

3.1. X-Ray Diffraction Study. Figure 1 shows the XRD spectra of CdTiO₃/PVP nanofiber mats. The nanofiber mats were dried at 200 °C in an oven for 1 h to remove the moisture and for easy removal of mats from the aluminum foil. The mats were then annealed at different temperatures for 3 h to remove the PVP and other solvents. The polycrystalline structure achieved at 600 °C is of the ilmenite rhombohedral phase with some impurity peaks of CdO. The peaks of CdO are present at $2\theta = 33.06$ and 38.34 as indicated in Figure 1a. The XRD pattern agrees with JCPDS Card no. 29-0277. The reflections were indexed in the ilmenite rhombohedral symmetry with lattice constant parameters a = 5.29 Å and c = 14.87 Å. To get a

pure ilmenite phase, we annealed the sample at different temperatures. We observed that at 950 °C the material yields the pure ilmenite phase. At this temperature, all of the traces of CdO are removed. The peaks shown in Figure 1b are indexed to the pure ilmenite phase of CdTiO₃ in space group $R\overline{3}$ (JCPDs card no. 29-0277). The presence of a new phase, recognized as orthorhombic CdTiO₃, was achieved at 1000 °C as shown in Figure 1c. At this temperature, no peaks of possible impurity phases such as TiO₂ and CdO are visible. All the diffraction peaks are indexed successfully according to the pure orthorhombic phase of CdTiO₃ with JCPDs card no. 78-1015 in space group *Pbn*21. The lattice constant parameters are a =5.30 Å, b = 5.32 Å, and c = 7.67 Å. Further annealing at 1100 $^{\circ}\text{C}$, the traces of rutile TiO_2 were observed in the orthorhombic CdTiO₃ as shown in Figure 1d. This may be due to the volatilization of cadmium at a relatively high temperature.²⁶ The sample annealed at 1200 °C shows the cadmium free pure rutile TiO₂ phase as shown in Figure 1e. All the diffraction peaks were indexed to a rutile phase of TiO₂ (JCPDs 72-1148) in space group P42/mnm. The lattice constant parameters are a = 4.59 Å and c = 2.96 Å. This confirms the complete cadmium volatilization.

The diffraction peaks in the X-ray patterns indicate a random or preferential growth of polycrystalline samples. To describe the preferential orientation, the texture coefficient (TC_{hkl}) was calculated by using equation²⁷

$$TC_{hkl} = \frac{I_{hkl}/I_{r(hkl)}}{1/n\sum_{n} (I_{hkl}/I_{r(hkl)})}$$
(1)

where I_{hkl} indicates the intensities obtained from the X-ray diffraction pattern of nanofiber mats and *n* is the number of diffraction peaks taken into account. $I_{r(hkl)}$ is the intensity of the reference pattern (JCPDs card). The deviation of TC_{*hkl*} from unity or higher value implies the growth in the preferred orientation. This means that the growth in the preferred orientation is associated with the increased number of grains along that plane.²⁸ TC_{*hkl*}'s calculated for the nanofiber mats of different phases are shown in Table S (Supporting Information). It can be seen from Table S that the highest value of TC_{*hkl*} obtained from the ilmenite phase (950 °C) is 1.49 associated with the (012) plane, the orthorhombic phase (1000 °C) is 1.26 associated with the (113) plane, and rutile TiO₂ (1200 °C) is 1.60 associated with the (002) plane.

3.2. SEM and TEM Study. Figure 2 shows the morphologies of the CdTiO₃ nanofibers as a function of annealing temperature. After annealing at 600 $^\circ$ C, the average diameter of the nanofibers is \sim 200 nm as shown in Figure 2a. The surface of the nanofibers annealed at this temperature is seen to be porous in nature. The HRTEM image of nanofibers annealed at 600 °C is shown in Figure 2b. From Figure 2b, it is observed that the nanofibers are composed of fine and closely linked grains ~ 25 nm in size. The HRTEM image (Figure 2b) shows well-resolved lattice fringes. The distance between the adjacent lattice fringes is 0.36 and 0.29 nm, which corresponds to the interplanar spacing of $CdTiO_3$ (012) and (104) planes, respectively. Which agrees well with the d (012) and (104) spacing of the literature value (0.38 and 0.28 nm; JCPDS no. 29-0277). The corresponding selected area electron diffraction (SAED) pattern (inset of Figure 2b) of the nanofibers indicates clearly that nanofibers are polycrystalline. All of the diffraction rings can be indexed to the ilmenite phase of CdTiO₃ with rhombohedral structure. Figure 2c and d shows the SEM image

of the sample annealed at 1000 and 1200 °C. The average diameter of nanofibers annealed at 1000 and 1200 °C is ~600 nm and ~800 nm, respectively. The inset of Figure 2c shows the TEM image of the sample annealed at 1000 °C. At an annealing temperature of 1000 and 1200 °C, the grain growth took place. The grain growth is pinned by thermal grooving in fibers. The grain size is about the same as the fiber diameter and leaves less pores as compared to 600 °C. The two mechanisms for thermal grooving were explained by Mullins.²⁹ One is the evaporation-condensation and the other is the surface diffusion. In our case, the nanofibers have a large pore size (~19 nm). It is reported that the diffusion rate is high on the surface with large pore size.³⁰ This can explain that the inner surfaces of the nanofibers are utilized for gas detection. Therefore, we believe that surface diffusion is dominant in our case. The same mechanism was also suggested for zirconia nanofibers.³¹

3.3. BET Characterization. The BET surface area values calculated are 9.41 and 0.4 m^2/g for ilmenite and perovskite phases, respectively. As expected, the high temperature calcination step has reduced the surface area and porosity of the material. Surface area determined using BET is closely related to the average diameter of the nanofibers. As the diameter increases, the specific surface area also decreases. The extracted parameters from BET data are shown in Table 1.

 Table 1. Surface Area, Pore Volume, Response Time, and
 Recovery Time for Both the Phases

sample	surface area (m²/g)	pore volume (cm ³ /g)	response time	recovery time
Ilmenite phase	9.41	0.04	~120 s	~23 s
Perovskite phase	0.40	0.02	~156 s	~50 s

3.4. Oxygen Sensing. Figure 4a and b shows room temperature I-V characteristics of CdTiO₃ nanofiber sensors at different oxygen flow rates. Greater flow rate means greater oxygen concentration in the measurement chamber. As oxygen flow rate increases, current decreases in both ilmenite and perovskite nanofiber sensors. However, at 2.5 V, the change in current is greater for the ilmenite nanofibers sensor as compared to that in the perovskite nanofibers sensor. Figure 4c shows the relationship between oxygen flow rate and current at 2 V.

The DC electrical measurements have been employed widely to investigate the electronic and sensing properties in different oxide nanostructures at room temperature.^{32–34} The hydrophilic surface of oxide nanofibers attracts hydrophilic contents (OH⁻, H₂O, O⁻, O₂⁻, and O₂) from the surrounding environment.³⁵ Increase in hydrophilic contents or adsorption of hydrophilic contents on the surface of nanofibers result in increased sensing properties.

Oxygen sensing is mainly due to the surface oxygen chemisorption, which causes the formation of oxygen adsorbate (acceptor like states) on the surface. The CdTiO₃ surface contains the number of oxygen related physisorption and chemisorption species (hydrophilic contents).²¹ The dominant species are atomic O⁻ and molecular O₂⁻ ions. Generally, below 150 °C, the molecular ions are dominant, whereas above this temperature the atomic ions take part^{36,37} in sensing. These dominant species are negatively ionized. In the case of *n*-type semiconductor metal oxide, oxygen chemisorption extracts

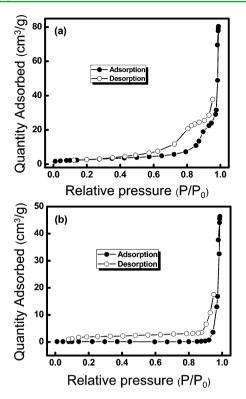


Figure 3. Nitrogen adsorption–desorption analysis of $CdTiO_3$ nanofibers annealed at (a) 600 °C and (b) 1000 °C.

electrons from the bulk and builds a space-charge layer (L) on the nanofibers surface. This creation of acceptor like states on the surface of CdTiO₃ can help in trapping of electrons. This causes a decrease in the majority carriers (electrons) that lead to an increase in electrical resistance.¹² The chemical reactions are described by the following equations:

$$O_2 (gas) \rightarrow O_2 (adsorbed)$$
 (2)

$$O_2 (adsorbed) + e^- \rightarrow O_2^- (adsorbed)$$
 (3)

$$O_2^-$$
 (adsorbed) + $e^- \rightarrow 2O^-$ (4)

$$O^- + e^- \to O^{2-} \tag{5}$$

The working and response of the sensor usually depend on the thickness of the space-charge layer (L) formed from the O⁻ and O_2^- ions and on the grain size or the crystallite size (D) of the sensing material. The relationship of crystallite size and space charge layer can be defined in three different following ways. (*i*) When the grain size of the material is small enough (D < 2L), conductivity will be controlled by the grain itself, and the surface conduction mechanism is dominant in this case. This condition is suitable in nanocrystalline materials for gas sensor applications.¹⁹ (*ii*) When crystalline size and space charge depth is comparable $(D \ge 2L)$, the space-charge depth around grains forms a restricted neck, and this neck acts as a potential barrier, and this makes conduction difficult. In this case, the conduction mechanism usually is controlled by the grain boundaries. (iii) When the grain size is large enough $(D \gg 2L)$, the conductivity will depend on the inner mobile charge carriers, and the conductivity depends on the barrier height.

The average grain size of the CdTiO₃ nanofibers with the ilmenite phase annealed at 600 °C is ~25 nm. The *L* of the chemisorbed oxygen range is normally ~ 10^2 to 10^3 nm for the

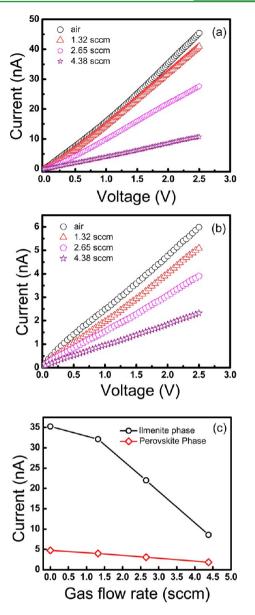


Figure 4. I-V characteristics of CdTiO₃ nanofibers gas sensing device at different oxygen flow rates. (a) Ilmenite phase, (b) perovskite phase, and (c) relationship between oxygen flow rate and current calculated at 2 V.

semiconducting oxide materials.³⁸ Hence, as discussed earlier, surface conduction is dominant in this case (D < 2L), and therefore the surface-to-bulk ratio of the material is much greater than that of coarse material.³⁹ Therefore, the grain size of the material is very important to controlling the gas sensing properties of the material. Upon annealing at 1000 °C, the material changes to neck control type $(D \ge 2L)$.^{40,41} So conduction is controlled by grain boundaries. Figure 5 shows the schematic representation of CdTiO₃ nanofibers showing the effect of the crystallite size on the sensitivity of a gas sensing device.

Gas response is defined as the ratio of the resistance change of a sensor upon exposure to a sample gas to its original resistance:

gas response =
$$\frac{R_g}{R_o} - 1 R_g > R_o$$
 (6)

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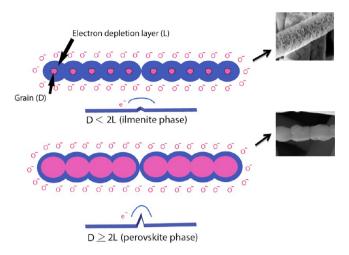


Figure 5. Schematic representation of $CdTiO_3$ nanofibers showing the effect of the crystallite size on the sensitivity of oxygen sensor sensing devices.

gas response =
$$1 - \frac{R_g}{R_o} R_o > R_g$$
 (7)

where R_0 is the resistance in air and R_g is the resistance in a sample gas.⁴¹ Figure 6a compares the gas response of ilmenite

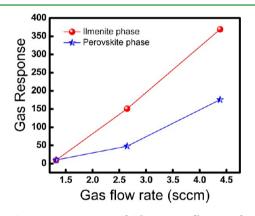


Figure 6. Gas response variation of $CdTiO_3$ nanofibers as a function of oxygen flow rates.

and perovskite CdTiO₃ nanofiber sensors at different oxygen flow rates. The gas response increased as the oxygen flow rate was increased for both the sensors. The perovskite nanofibers sensor showed a nonlinear response, whereas the ilmenite nanofibers sensor exhibited a linear response. At 4.38 sccm, the ilmenite nanofibers sensor exhibited a higher response as compared to the perovskite nanofibers sensor. This may be due to an increase in grain size and reduced pore size upon annealing at a temperature of 1000 °C. This also affects charge carrier concentration on the nanofiber surface.¹² The linear relationship between gas response and oxygen flow rate provides strong evidence for the availability of a sufficient number of sensing sites on the surface of nanofibers to interact with the oxygen.⁴² In addition, the surface reaction increases with an increase in oxygen flow rate due to a large surface coverage. It can also be concluded from the linearity of the response curve with the oxygen flow rate that the sensor can be reliably used to monitor oxygen over this range.⁴³

For practical applications, the response and recovery times of the gas sensors are very important. The response and recovery times of nanofiber sensors were recorded at 25 °C and 2 V and at an oxygen flow rate of 2.65 sccm. A complete recovery was observed after the removal of oxygen from the chamber. Figure 7a and b shows response time ($t_{(air-to-oxygen)}$) and recovery time

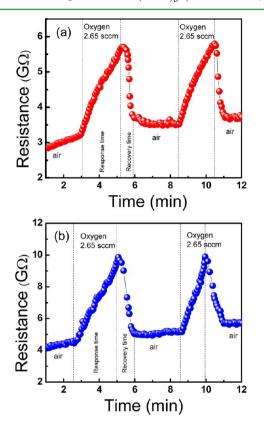


Figure 7. Response curves of $CdTiO_3$ nanofibers. (a) Ilmenite phase. (b) Perovskite phase.

 $(t_{(oxygen-to-air)})$ for both the ilmenite and perovskite phases. It can be seen that results are reproducible for two complete response/recovery cycles. The response time and recovery time for both phases of nanofibers are listed in Table 1.

4. CONCLUSIONS

The phase transformations in CdTiO₃ nanofibers upon thermal annealing at different temperatures were studied. The pure ilmenite phase was achieved at 950 °C, whereas annealing at 1000 °C resulted in the pure perovskite phase. CdTiO₃ nanofibers were converted to the TiO2 rutile phase at temperatures above 1100 °C. BET analysis indicated that the surface area of nanofibers decreases with an increase in annealing temperature. Oxygen sensors of CdTiO₃ nanofibers annealed at 600 °C (ilmenite) and 1000 °C (perovskite) were fabricated. Annealing caused changes in grain size, surface area, and porosity of nanofibers and therefore influenced the sensing properties of these nanofibers. The sensor based on ilmenite nanofibers (annealed at 600 °C) having a smaller grain size and higher surface area $(9.41 \text{ m}^2/\text{g})$ was more sensitive and had a fast response as compared to the sensor based on perovskite nanofibers (annealed at 1000 °C). On exposure to gas, the adsorption of oxygen ions on the nanofiber surface reduces the electrons for conduction, causing an increase in resistance of the nanofibers. These results demonstrate that CdTiO₃ nanofibers with the ilmenite phase could be promising candidates for the fabrication of oxygen sensors.

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ASSOCIATED CONTENT

S Supporting Information

X-ray diffraction intensities and preferred orientation factor for ilmenite phase $CdTiO_3$, perovskite phase $CdTiO_3$, and TiO_2 . This material is available free of charge via the Internet at http://pubs.acs.org.

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Notes

The authors declare no competing financial interest.

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4549